

DICIG
Marine Group

Seaborn Pile Driving
Lake Washington
Timber Pile Cap Analysis

Calculations Prepared For
Seaborn Pile Driving
7/14/2023

Prepared By: D. Truong
Reviewed By: J. Smoot

7422 East Mercer Way,
Mercer Island, WA

Cover Sheet

Calculation Narrative



The purpose of this calculation is to determine the structural capacity of steel channels used to brace existing timber pile caps located on Mercer Island, WA. The timber caps support timber stringers and decking for a recreational private dock. Loading and structural capacity of the caps were analyzed using ASCE 7-10 and AWC NDS 2018, respectively. The pile cap with the longest span is the controlling case as all the pile caps have similar loading and structural properties. All dimensions are estimated based on photos provided by Seaborn Pile Driving. Timber is assumed to have full capacity.

A point load is applied to the end of the cantilever by a neighboring dock. Enercalc is used to evaluate the overhanging beam to determine the max shear and moment demand.

The engineer of record certifies the correctness of all calculations herein with the stamp affixed below. A thorough review of all structural components identified in the load cases on page 2 to be those critical for the performance and safety of the structure





**Seaborn Pile Driving
Lake Washington
Timber Pile Cap Analysis**

**Calculations Prepared For
Seaborn Pile Driving
7/14/2023**

**Prepared By: D. Truong
Reviewed By: J. Smoot**

**7422 East Mercer Way,
Mercer Island, WA**

Calculation Summary

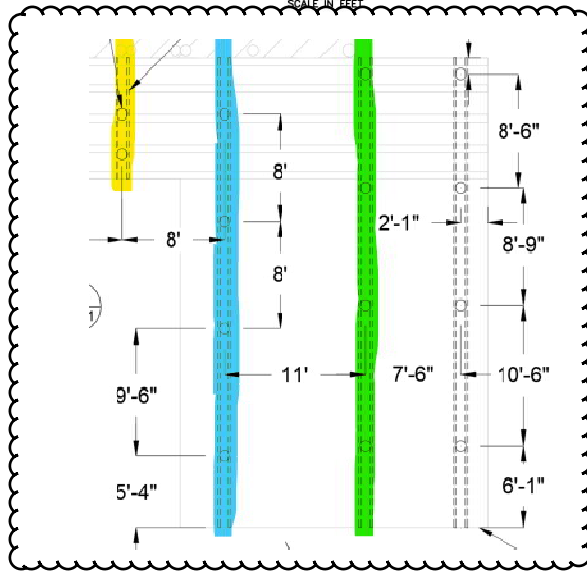
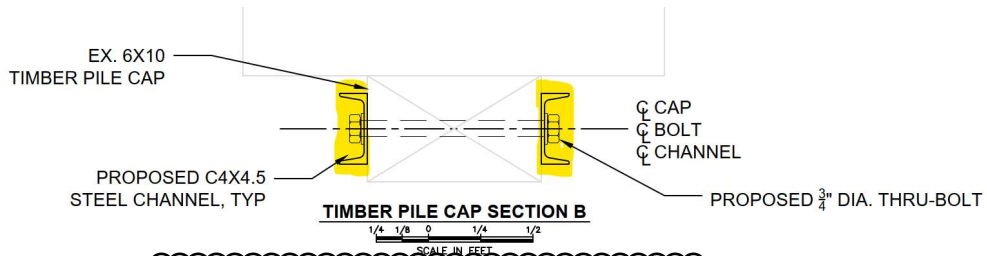
Vertical Loading Summary


Structural Component	Page #	Shear Dem. (Kip)	Shear Cap. (Kip)	DCR	Mom. Dem. (Kip-ft)	Mom. Cap. (Kip-ft)	DCR	Defl. (in)	Defl. Crit. L/360 (in)	DCR
Double Channel C4x4.5, Pile Cap 1	5-8	3.4	18	OK	8.6	13	OK			
Double Channel C4x4.5, Pile Cap 2	9-12	3.4	18	OK	9.2	13	OK			
Double Channel C4x4.5, Pile Cap 3	13-16	4.2	18	OK	12.0	13	OK			
Double Channel Thru Bolt	17	0.9	1.8	OK						

Summary

**Double Channel Design
Connection**

**(2) C4x4.5, Both Sides of Beam
(2) 3/4" Ø Thru Bolt**




	Seaborn Pile Driving Lake Washington Timber Pile Cap Analysis	Calculations Prepared For Seaborn Pile Driving 7/14/2023
---	--	---

Prepared By: D. Truong Reviewed By: J. Smoot	7422 East Mercer Way, Mercer Island, WA	Timber Cap Demand
---	--	--------------------------

6" x 10" Timber Cap Dead Load

Component	Tributary L (ft)	W (in)	D (in)	Unit Weight (lbs/ft (SF))	Quant. (ea)	WEIGHT (plf)
<u>Distributed Dead Loads</u>						
6" x 10" Timber Cap	13	9.5	5.5	5.3	1	68.9
2" x 8" Timber Decking	10	7.5	1.5	3	1	48.0
4" x 12" PT Timber Stringer	9	3.5	11.25	10.9	6	72.9
					Total	189.8

6" x 10" Timber Cap Live Load

Tributary Width	10 ft		
Live Load	40 psf	Mercer Island Code	
Total Load	400 plf		

Snow Load


Ce	Exposure Factor	0.9	ASCE Table 7.3-1
Ct	Thermal Factor	1.2	ASCE Table 7.3-2
Cs	Slope Factor	1	ASCE Fig. 7.4-1
pg	Ground Snow Load	28 psf	ASCE Hazard Tool
pf	Flat Roof Snow Load	21.2 psf	ASCE 7.3-1
ps	Sloped Roof Snow Load	21.2 psf	ASCE 7.4-1
ws	Snow Line Load	212 plf	


Point Load from neighboring Dock

Dead Load	0.21 kip	
Live Load	0.66 kip	
NOTE: This load is set on the end of the cantilever		

Load Combination (Allowable Stress Design)

1.0 D + 1.0 L	0.59 klf	ASCE Ch 2.4.1
1.0 D + 0.75 L + 0.75 S	0.65 klf	ASCE Ch 2.4.1
Max Shear, Vmax	4.2 kip	Enercalc
Max Moment, Mmax	12 kip-ft	Enercalc





Seaborn Pile Driving
Lake Washington
Timber Pile Cap Analysis

Calculations Prepared For
Seaborn Pile Driving
7/14/2023

Prepared By: D. Truong
Reviewed By: J. Smoot

7422 East Mercer Way,
Mercer Island, WA

Timber Cap Capacity

6" x 10" Timber Cap Bending Capacity

F _b	875 psi	Doug Fir No. 2
C _D	1	Live Load NDS Table 2.3.2
C _M	1	mc >16%, Table 5A
C _t	1	T<100, NDS Table 2.3.3
C _i	0.8	Cap has incising
C _L	1	d<b
C _F	1	d<12"
C _{fu}	1	Loaded on wide face
C _c	1	

Table 4.3.1 Applicability of Adjustment Factors for Sawn Lumber

	ASD only	ASD and LRFD										
		Load Duration Factor	Wet Service Factor	Temperature Factor	Beam Stability Factor	Size Factor	Flat Use Factor	Incising Factor	Repetitive Member Factor	Column Stability Factor	Backing Stiffness Factor	Beating Area Factor
F _b = F _b	x	C _D	C _M	C _t	C _L	C _F	C _{fu}	C _i	C _r	-	-	-
F _t = F _t	x	C _D	C _M	C _t	-	C _F	-	C _i	-	-	-	-
F _v = F _v	x	C _D	C _M	C _t	-	-	-	C _i	-	-	-	-

Bending Capacity

F _b '	700 psi
S _x	48 in ³
M _n	2.8 kip-ft

Section Modulus

F_b & F_v Reference Design Values

DOUGLAS FIR-LARCH												
Dense Select Structural		1,800	1,100	170	730	1,300	1,700,000	820,000				
Select Structural		1,600	950	170	625	1,100	1,600,000	580,000				
Dense No. 1	Beams and Stringers	1,550	775	170	730	1,100	1,700,000	820,000				
No. 1		1,350	675	170	625	925	1,600,000	580,000				
No. 2		875	425	170	625	600	1,300,000	470,000				0.50

Bending Demand

M _{max}	12 kip-ft
DCR	4.3 NG

Moment Demand

Timber Cap Alone is not Structurally Sound

6" x 10" Timber Cap Shear Capacity

F _v	170 psi	Doug Fir No. 2
C _D	1	Live Load NDS Table 2.3.2
C _M	0.8	mc >16%, Table 5A
C _t	1	T<100, NDS Table 2.3.3
C _i	0.8	Cap has incising

Allowable Shear Stress

F _v '	108.8 psi
A	52.25 in ²
V _n	5.7 kip

Cross Sectional Area

Actual Shear Stress

V _{max}	4.2 kips
------------------	----------

Shear Demand

DCR 0.7 GOOD OK

Steel Beam

Project File: Liu.ec6

LIC# : KW-06012482, Build:20.23.2.14

Davido Consulting Group

(c) ENERCALC INC 1983-2022

DESCRIPTION: C4x4.5 Pile Cap Type 1

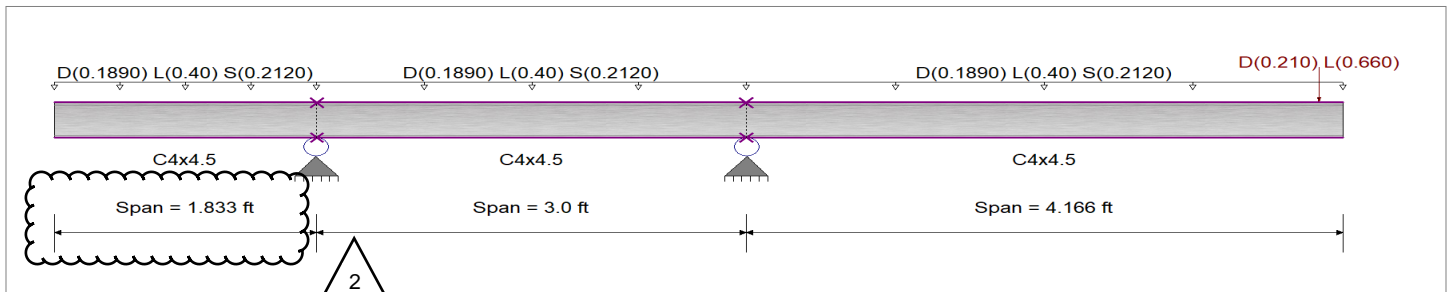
CODE REFERENCES

Calculations per AISC 360-16, IBC 2018, CBC 2019, ASCE 7-16
 Load Combination Set : IBC 2021

Material Properties

Analysis Method Allowable Strength Design
 Beam Bracing : Beam is Fully Braced against lateral-torsional buckling
 Bending Axis : Major Axis Bending

Fy : Steel Yield : 50.0 ksi
 E: Modulus : 29,000.0 ksi



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight NOT internally calculated and added
 Load for Span Number 1

Uniform Load : D = 0.1890, L = 0.40, S = 0.2120 k/ft, Tributary Width = 1.0 ft

Load for Span Number 2

Uniform Load : D = 0.1890, L = 0.40, S = 0.2120 k/ft, Tributary Width = 1.0 ft

Load for Span Number 3

Uniform Load : D = 0.1890, L = 0.40, S = 0.2120 k/ft, Tributary Width = 1.0 ft

Point Load : D = 0.210, L = 0.660 k @ 4.0 ft

**Timber Cap + Double Channel
 DCR = 0.66**

DESIGN SUMMARY

				Design N.G.			
Maximum Bending Stress Ratio =	1.680	: 1	Maximum Shear Stress Ratio =	0.381	: 1		
Section used for this span	C4x4.5		Section used for this span	C4x4.5			
Ma : Applied	8.591 k-ft		Va : Applied	3.424 k			
Mn / Omega : Allowable	5.115 k-ft		Vn/Omega : Allowable	8.982 k			
Load Combination	+D+L		Load Combination	+D+0.750L+0.750S			
Span # where maximum occurs	Span # 2		Location of maximum on span	3.000 ft			
			Span # where maximum occurs	Span # 2			

Maximum Deflection

Max Downward Transient Deflection	0.926 in	Ratio =	107	>=	Span : 3 : L Only
Max Upward Transient Deflection	-0.059 in	Ratio =	609	>=	Span : 3 : L Only
Max Downward Total Deflection	1.296 in	Ratio =	77	>=	Span : 3 : +D+L
Max Upward Total Deflection	-0.083 in	Ratio =	434	>=	Span : 3 : +D+L

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios		Summary of Moment Values					Summary of Shear Values				
			M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx/Vnx/Omega	
D Only														
Dsgn. L =	1.83 ft	1	0.062	0.049		-0.32	0.32	8.54	5.11	1.00	1.00	0.44	15.00	8.98
Dsgn. L =	3.00 ft	2	0.485	0.112	-0.00	-2.48	2.48	8.54	5.11	1.00	1.00	1.00	15.00	8.98
Dsgn. L =	4.17 ft	3	0.485	0.111		-2.48	2.48	8.54	5.11	1.00	1.00	1.00	15.00	8.98
+D+L														
Dsgn. L =	1.83 ft	1	0.193	0.184		-0.99	0.99	8.54	5.11	1.00	1.00	1.65	15.00	8.98
Dsgn. L =	3.00 ft	2	1.680	0.380	-0.00	-8.59	8.59	8.54	5.11	1.00	1.00	3.42	15.00	8.98
Dsgn. L =	4.17 ft	3	1.680	0.370		-8.59	8.59	8.54	5.11	1.00	1.00	3.32	15.00	8.98
+D+S														
Dsgn. L =	1.83 ft	1	0.132	0.082		-0.67	0.67	8.54	5.11	1.00	1.00	0.74	15.00	8.98
Dsgn. L =	3.00 ft	2	0.845	0.209	-0.00	-4.32	4.32	8.54	5.11	1.00	1.00	1.88	15.00	8.98

Steel Beam

Project File: Liu.ec6

LIC# : KW-06012482, Build:20.23.2.14

Davido Consulting Group

(c) ENERCALC INC 1983-2022

DESCRIPTION: C4x4.5 Pile Cap Type 1

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios		Summary of Moment Values					Summary of Shear Values				
			M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega Cb	Rm	Va Max	Vnx/Vnx/Omega		
Dsgn. L = 4.17 ft	4.17 ft	3	0.845	0.209		-4.32	4.32	8.54	5.11	1.00	1.00	1.88	15.00	8.98
+D+0.750L														
Dsgn. L = 1.83 ft	1.83 ft	1	0.161	0.150		-0.82	0.82	8.54	5.11	1.00	1.00	1.35	15.00	8.98
Dsgn. L = 3.00 ft	3.00 ft	2	1.381	0.313	-0.00	-7.06	7.06	8.54	5.11	1.00	1.00	2.81	15.00	8.98
Dsgn. L = 4.17 ft	4.17 ft	3	1.381	0.305		-7.06	7.06	8.54	5.11	1.00	1.00	2.74	15.00	8.98
+D+0.750L+0.750S														
Dsgn. L = 1.83 ft	1.83 ft	1	0.213	0.165		-1.09	1.09	8.54	5.11	1.00	1.00	1.48	15.00	8.98
Dsgn. L = 3.00 ft	3.00 ft	2	1.651	0.381	-0.00	-8.44	8.44	8.54	5.11	1.00	1.00	3.42	15.00	8.98
Dsgn. L = 4.17 ft	4.17 ft	3	1.651	0.379		-8.44	8.44	8.54	5.11	1.00	1.00	3.40	15.00	8.98
+0.60D														
Dsgn. L = 1.83 ft	1.83 ft	1	0.037	0.029		-0.19	0.19	8.54	5.11	1.00	1.00	0.26	15.00	8.98
Dsgn. L = 3.00 ft	3.00 ft	2	0.291	0.067	-0.00	-1.49	1.49	8.54	5.11	1.00	1.00	0.60	15.00	8.98
Dsgn. L = 4.17 ft	4.17 ft	3	0.291	0.067		-1.49	1.49	8.54	5.11	1.00	1.00	0.60	15.00	8.98

Vertical Reactions

Support notation : Far left is #

Values in KIPS

Load Combination	Support 1	Support 2	Support 3	Support 4
Max Upward from all Load Conditions		0.212	6.828	0.972
Max Upward from Load Combinations		0.121	6.828	0.972
Max Upward from Load Cases		0.212	4.739	0.972
Max Downward from all Load Conditions (Resi:		-0.571		0.972
Max Downward from Load Combinations (Resi		-0.571		0.972
Max Downward from Load Cases (Resisting U _j		-0.480		0.972
D Only		-0.091	2.002	0.972
+D+L		-0.571	6.741	0.972
+D+S		0.121	3.697	0.972
+D+0.750L		-0.451	5.556	0.972
+D+0.750L+0.750S		-0.292	6.828	0.972
+0.60D		-0.055	1.201	0.972
L Only		-0.480	4.739	0.972
S Only		0.212	1.696	0.972

Steel Section Properties : C4x4.5

Depth	=	4.000 in	I _{xx}	=	3.53 in ⁴	J	=	0.031 in ⁴
Web Thick	=	0.125 in	S _{xx}	=	1.77 in ³	C _w	=	0.78 in ⁶
Flange Width	=	1.520 in	R _{xx}	=	1.620 in	R _p	=	1.970 in
Flange Thick	=	0.296 in	Z _x	=	2.050 in ³	H	=	0.727 in
Area	=	1.340 in ²	I _{yy}	=	0.265 in ⁴	W _{no}	=	1.550 in ²
Weight	=	4.500 plf	S _{yy}	=	0.253 in ³	Sw	=	0.193 in ⁴
Kdesign	=	0.750 in	R _{yy}	=	0.445 in	Q _f	=	0.765 in ³
			Z _y	=	0.495 in ³	Q _w	=	1.010 in ³
r _{ts}	=	0.506 in				W _{n2}	=	0.000
Y _{cg}	=	2.000 in				Sw ₂	=	0.088
X _{cg}	=	0.473 in				Sw ₃	=	0.044
X _p	=	0.305 in						
E _o	=	0.556 in						

Steel Beam

Project File: Liu.ec6

LIC# : KW-06012482, Build:20.23.2.14

Davido Consulting Group

(c) ENERCALC INC 1983-2022

DESCRIPTION: C4x4.5 Pile Cap Type 1

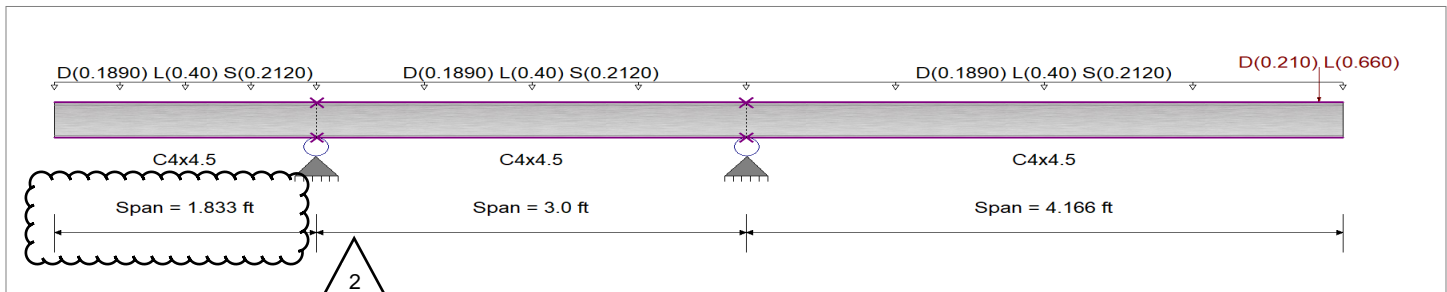
CODE REFERENCES

Calculations per AISC 360-16, IBC 2018, CBC 2019, ASCE 7-16
 Load Combination Set : IBC 2021

Material Properties

Analysis Method Allowable Strength Design
 Beam Bracing : Beam is Fully Braced against lateral-torsional buckling
 Bending Axis : Major Axis Bending

Fy : Steel Yield : 50.0 ksi
 E: Modulus : 29,000.0 ksi



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight NOT internally calculated and added
 Load for Span Number 1

Uniform Load : D = 0.1890, L = 0.40, S = 0.2120 k/ft, Tributary Width = 1.0 ft

Load for Span Number 2

Uniform Load : D = 0.1890, L = 0.40, S = 0.2120 k/ft, Tributary Width = 1.0 ft

Load for Span Number 3

Uniform Load : D = 0.1890, L = 0.40, S = 0.2120 k/ft, Tributary Width = 1.0 ft

Point Load : D = 0.210, L = 0.660 k @ 4.0 ft

**Timber Cap + Double Channel
 DCR = 0.66**

DESIGN SUMMARY

				Design N.G.			
Maximum Bending Stress Ratio =	1.680	: 1	Maximum Shear Stress Ratio =	0.381	: 1		
Section used for this span	C4x4.5		Section used for this span	C4x4.5			
Ma : Applied	8.591 k-ft		Va : Applied	3.424 k			
Mn / Omega : Allowable	5.115 k-ft		Vn/Omega : Allowable	8.982 k			
Load Combination	+D+L		Load Combination	+D+0.750L+0.750S			
Span # where maximum occurs	Span # 2		Location of maximum on span	3.000 ft			
			Span # where maximum occurs	Span # 2			

Maximum Deflection

Max Downward Transient Deflection	0.926 in	Ratio =	107	>=	Span: 3 : L Only
Max Upward Transient Deflection	-0.059 in	Ratio =	609	>=	Span: 3 : L Only
Max Downward Total Deflection	1.296 in	Ratio =	77	>=	Span: 3 : +D+L
Max Upward Total Deflection	-0.083 in	Ratio =	434	>=	Span: 3 : +D+L

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios		Summary of Moment Values					Summary of Shear Values				
			M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx/Vnx/Omega	
D Only														
Dsgn. L =	1.83 ft	1	0.062	0.049		-0.32	0.32	8.54	5.11	1.00	1.00	0.44	15.00	8.98
Dsgn. L =	3.00 ft	2	0.485	0.112	-0.00	-2.48	2.48	8.54	5.11	1.00	1.00	1.00	15.00	8.98
Dsgn. L =	4.17 ft	3	0.485	0.111		-2.48	2.48	8.54	5.11	1.00	1.00	1.00	15.00	8.98
+D+L														
Dsgn. L =	1.83 ft	1	0.193	0.184		-0.99	0.99	8.54	5.11	1.00	1.00	1.65	15.00	8.98
Dsgn. L =	3.00 ft	2	1.680	0.380	-0.00	-8.59	8.59	8.54	5.11	1.00	1.00	3.42	15.00	8.98
Dsgn. L =	4.17 ft	3	1.680	0.370		-8.59	8.59	8.54	5.11	1.00	1.00	3.32	15.00	8.98
+D+S														
Dsgn. L =	1.83 ft	1	0.132	0.082		-0.67	0.67	8.54	5.11	1.00	1.00	0.74	15.00	8.98
Dsgn. L =	3.00 ft	2	0.845	0.209	-0.00	-4.32	4.32	8.54	5.11	1.00	1.00	1.88	15.00	8.98

Steel Beam

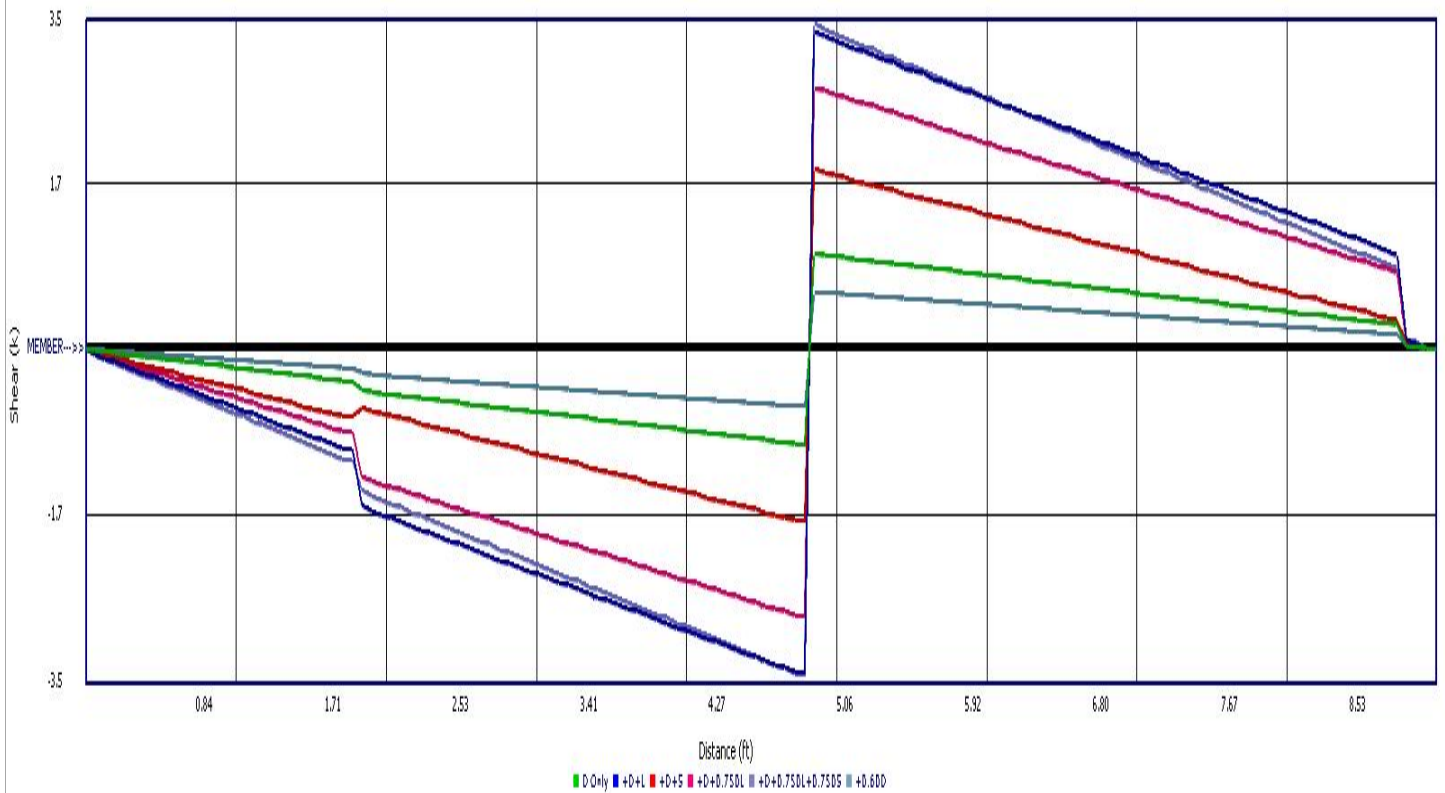
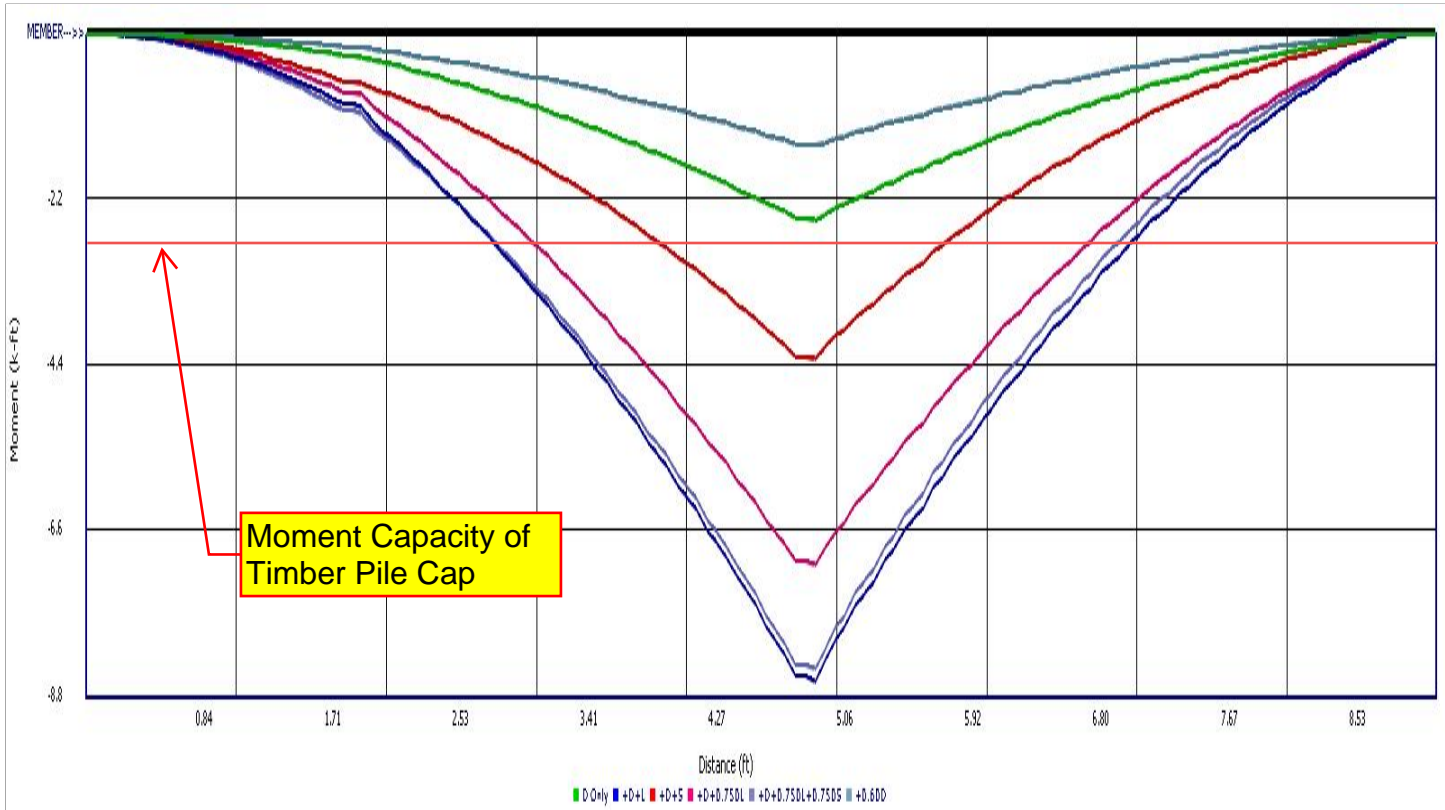
Project File: Liu.ec6

LIC# : KW-06012482, Build:20.23.2.14

Davido Consulting Group

(c) ENERCALC INC 1983-2022

DESCRIPTION: C4x4.5 Pile Cap Type 1



Steel Beam

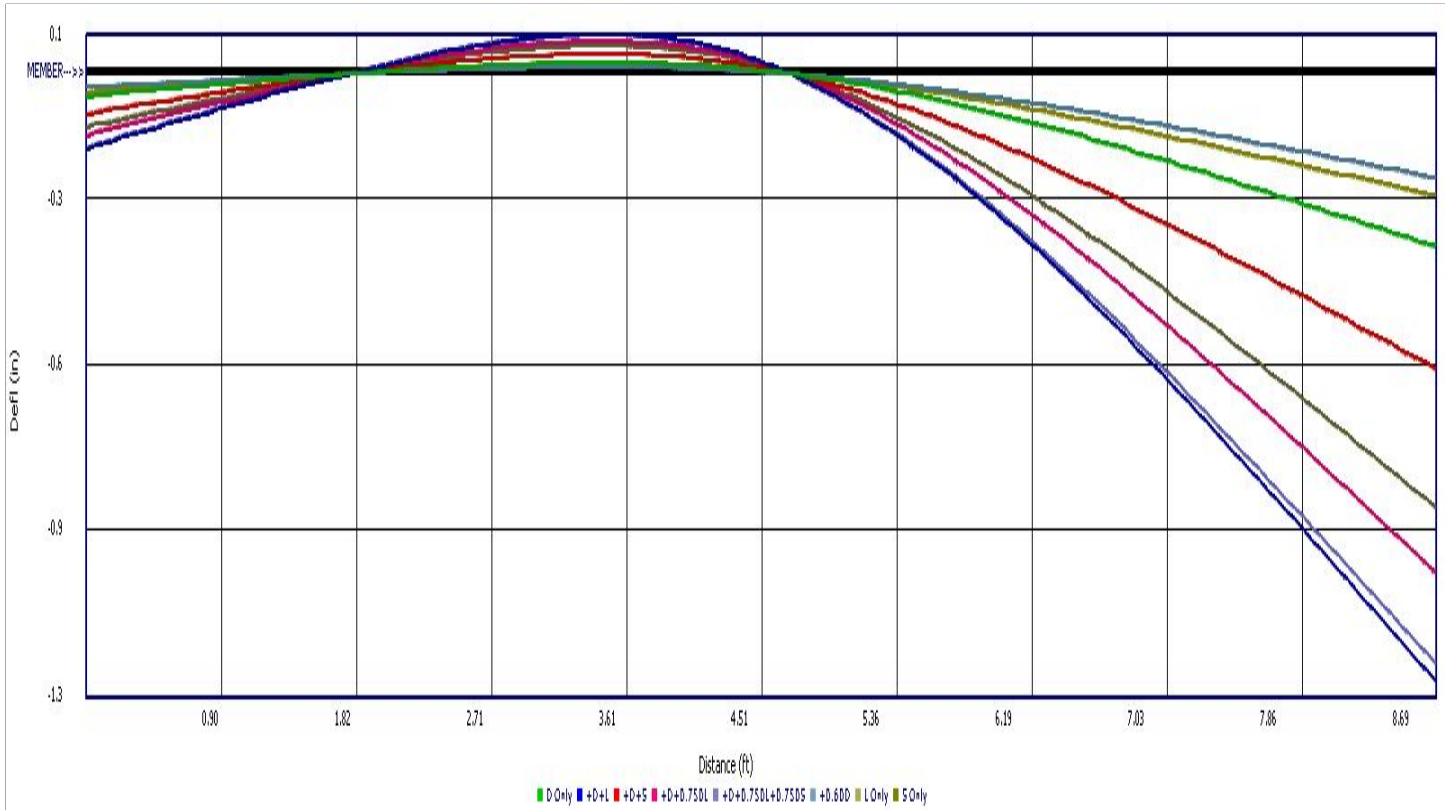
Project File: Liu.ec6

LIC# : KW-06012482, Build:20.23.2.14

Davido Consulting Group

(c) ENERCALC INC 1983-2022

DESCRIPTION: C4x4.5 Pile Cap Type 1



Steel Beam

Project File: Liu.ec6

LIC# : KW-06012482, Build:20.23.2.14

Davido Consulting Group

(c) ENERCALC INC 1983-2022

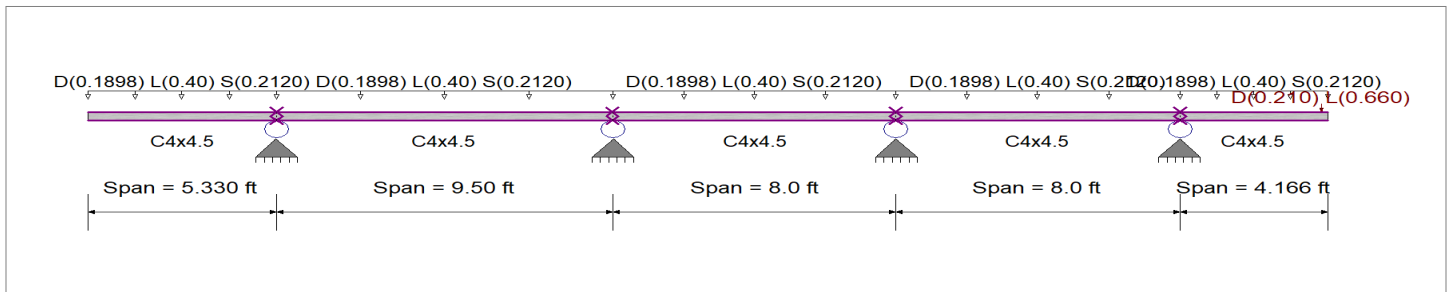
DESCRIPTION: C4x4.5 Pile Cap Type 2

CODE REFERENCES

Calculations per AISC 360-16, IBC 2018, CBC 2019, ASCE 7-16
 Load Combination Set : IBC 2021

Material Properties

Analysis Method Allowable Strength Design
 Beam Bracing : Beam is Fully Braced against lateral-torsional buckling
 Bending Axis : Major Axis Bending
 Fy : Steel Yield : 50.0 ksi
 E: Modulus : 29,000.0 ksi



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight NOT internally calculated and added

Load for Span Number 1

Uniform Load : D = 0.1898, L = 0.40, S = 0.2120 k/ft, Tributary Width = 1.0 ft

Load for Span Number 2

Uniform Load : D = 0.1898, L = 0.40, S = 0.2120 k/ft, Tributary Width = 1.0 ft

Load for Span Number 3

Uniform Load : D = 0.1898, L = 0.40, S = 0.2120 k/ft, Tributary Width = 1.0 ft

Load for Span Number 4

Uniform Load : D = 0.1898, L = 0.40, S = 0.2120 k/ft, Tributary Width = 1.0 ft

Load for Span Number 5

Uniform Load : D = 0.1898, L = 0.40, S = 0.2120 k/ft, Tributary Width = 1.0 ft

Point Load : D = 0.210, L = 0.660 k @ 4.0 ft

**Timber Cap + Double Channel
 DCR = 0.707**

DESIGN SUMMARY

Design N.G.

Maximum Bending Stress Ratio =	1.802 : 1	Maximum Shear Stress Ratio =	0.412 : 1
Section used for this span	C4x4.5	Section used for this span	C4x4.5
Ma : Applied	9.216 k-ft	Va : Applied	3.701 k
Mn / Omega : Allowable	5.115 k-ft	Vn/Omega : Allowable	8.982 k
Load Combination	+D+0.750L+0.750S	Load Combination	+D+0.750L+0.750S
Span # where maximum occurs	Span # 1	Location of maximum on span	5.330 ft
		Span # where maximum occurs	Span # 1
Maximum Deflection			
Max Downward Transient Deflection	1.157 in Ratio =	86	>= Span: 5 : L Only
Max Upward Transient Deflection	-0.158 in Ratio =	608	>= Span: 5 : L Only
Max Downward Total Deflection	2.126 in Ratio =	60	>= Span: 5 : +D+0.750L+0.750S
Max Upward Total Deflection	-0.211 in Ratio =	454	>= Span: 5 : +D+L

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios		Summary of Moment Values					Summary of Shear Values				
			M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx/Vnx/Omega	
D Only														
Dsgn. L =	5.33 ft	1	0.527	0.121		-2.70	2.70	8.54	5.11	1.00	1.00	1.08	15.00	8.98
Dsgn. L =	9.50 ft	2	0.527	0.121	0.39	-2.70	2.70	8.54	5.11	1.00	1.00	1.08	15.00	8.98
Dsgn. L =	8.00 ft	3	0.191	0.089	0.71	-0.98	0.98	8.54	5.11	1.00	1.00	0.80	15.00	8.98

Steel Beam

Project File: Liu.ec6

LIC# : KW-06012482, Build:20.23.2.14

Davido Consulting Group

(c) ENERCALC INC 1983-2022

DESCRIPTION: C4x4.5 Pile Cap Type 2

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios		Summary of Moment Values					Summary of Shear Values				
			M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega Cb	Rm	Va Max	Vnx/Vnx/Omega		
Dsgn. L =	8.00 ft	4	0.486	0.111	0.09	-2.49	2.49	8.54	5.11	1.00	1.00	1.00	15.00	8.98
Dsgn. L =	4.17 ft	5	0.486	0.111		-2.49	2.49	8.54	5.11	1.00	1.00	1.00	15.00	8.98
+D+L														
Dsgn. L =	5.33 ft	1	1.638	0.374		-8.38	8.38	8.54	5.11	1.00	1.00	3.36	15.00	8.98
Dsgn. L =	9.50 ft	2	1.638	0.374	1.19	-8.38	8.38	8.54	5.11	1.00	1.00	3.36	15.00	8.98
Dsgn. L =	8.00 ft	3	0.603	0.281	2.30	-3.08	3.08	8.54	5.11	1.00	1.00	2.52	15.00	8.98
Dsgn. L =	8.00 ft	4	1.681	0.370	0.13	-8.60	8.60	8.54	5.11	1.00	1.00	3.33	15.00	8.98
Dsgn. L =	4.17 ft	5	1.681	0.370		-8.60	8.60	8.54	5.11	1.00	1.00	3.33	15.00	8.98
+D+S														
Dsgn. L =	5.33 ft	1	1.116	0.256		-5.71	5.71	8.54	5.11	1.00	1.00	2.30	15.00	8.98
Dsgn. L =	9.50 ft	2	1.116	0.256	0.86	-5.71	5.71	8.54	5.11	1.00	1.00	2.30	15.00	8.98
Dsgn. L =	8.00 ft	3	0.393	0.184	1.40	-2.01	2.01	8.54	5.11	1.00	1.00	1.65	15.00	8.98
Dsgn. L =	8.00 ft	4	0.846	0.216	0.38	-4.33	4.33	8.54	5.11	1.00	1.00	1.94	15.00	8.98
Dsgn. L =	4.17 ft	5	0.846	0.210		-4.33	4.33	8.54	5.11	1.00	1.00	1.88	15.00	8.98
+D+0.750L														
Dsgn. L =	5.33 ft	1	1.360	0.311		-6.96	6.96	8.54	5.11	1.00	1.00	2.79	15.00	8.98
Dsgn. L =	9.50 ft	2	1.360	0.311	0.99	-6.96	6.96	8.54	5.11	1.00	1.00	2.79	15.00	8.98
Dsgn. L =	8.00 ft	3	0.500	0.233	1.90	-2.56	2.56	8.54	5.11	1.00	1.00	2.09	15.00	8.98
Dsgn. L =	8.00 ft	4	1.382	0.306	0.12	-7.07	7.07	8.54	5.11	1.00	1.00	2.75	15.00	8.98
Dsgn. L =	4.17 ft	5	1.382	0.306		-7.07	7.07	8.54	5.11	1.00	1.00	2.75	15.00	8.98
+D+0.750L+0.750S														
Dsgn. L =	5.33 ft	1	1.802	0.412		-9.22	9.22	8.54	5.11	1.00	1.00	3.70	15.00	8.98
Dsgn. L =	9.50 ft	2	1.802	0.412	1.34	-9.22	9.22	8.54	5.11	1.00	1.00	3.70	15.00	8.98
Dsgn. L =	8.00 ft	3	0.651	0.304	2.42	-3.33	3.33	8.54	5.11	1.00	1.00	2.73	15.00	8.98
Dsgn. L =	8.00 ft	4	1.652	0.379	0.31	-8.45	8.45	8.54	5.11	1.00	1.00	3.41	15.00	8.98
Dsgn. L =	4.17 ft	5	1.652	0.379		-8.45	8.45	8.54	5.11	1.00	1.00	3.41	15.00	8.98
+0.60D														
Dsgn. L =	5.33 ft	1	0.316	0.072		-1.62	1.62	8.54	5.11	1.00	1.00	0.65	15.00	8.98
Dsgn. L =	9.50 ft	2	0.316	0.072	0.24	-1.62	1.62	8.54	5.11	1.00	1.00	0.65	15.00	8.98
Dsgn. L =	8.00 ft	3	0.114	0.053	0.43	-0.59	0.59	8.54	5.11	1.00	1.00	0.48	15.00	8.98
Dsgn. L =	8.00 ft	4	0.292	0.067	0.05	-1.49	1.49	8.54	5.11	1.00	1.00	0.60	15.00	8.98
Dsgn. L =	4.17 ft	5	0.292	0.067		-1.49	1.49	8.54	5.11	1.00	1.00	0.60	15.00	8.98

Vertical Reactions

Support notation : Far left is #

Values in KIPS

Load Combination	Support 1	Support 2	Support 3	Support 4	Support 5	Support 6
Max Upward from all Load Conditions	7.159	5.193	4.279	6.779		
Max Upward from Load Combinations	7.159	5.193	4.279	6.779		
Max Upward from Load Cases	4.408	3.244	2.459	4.547		
D Only	2.094	1.520	1.249	1.989		
+D+L	6.502	4.764	3.708	6.536		
+D+S	4.440	3.174	2.830	3.828		
+D+0.750L	5.400	3.953	3.093	5.400		
+D+0.750L+0.750S	7.159	5.193	4.279	6.779		
+0.60D	1.257	0.912	0.749	1.194		
L Only	4.408	3.244	2.459	4.547		
S Only	2.345	1.654	1.581	1.839		

Steel Beam

Project File: Liu.ec6

LIC# : KW-06012482, Build:20.23.2.14

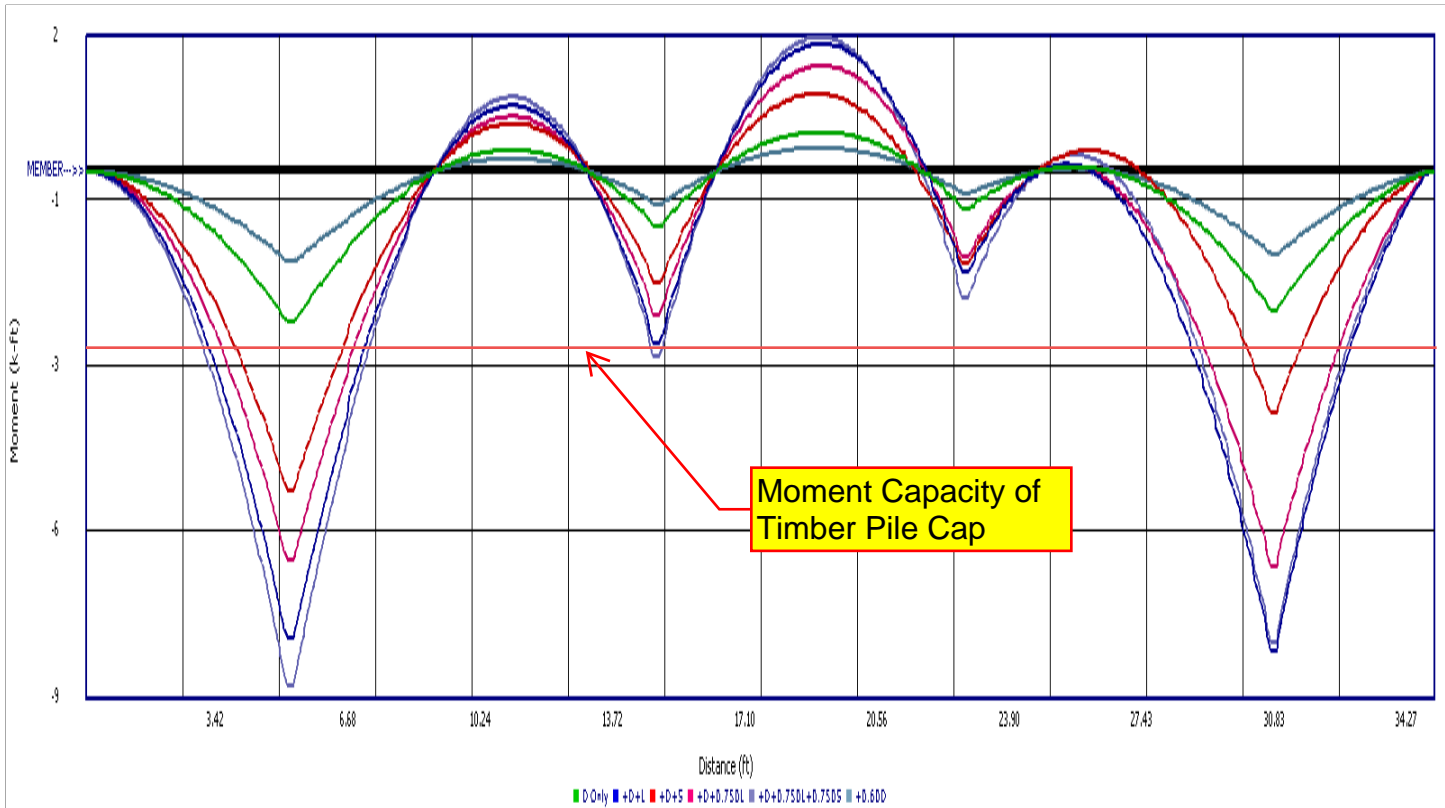
Davido Consulting Group

(c) ENERCALC INC 1983-2022

DESCRIPTION: C4x4.5 Pile Cap Type 2

Steel Section Properties : C4x4.5

Depth	=	4.000 in	I _{xx}	=	3.53 in ⁴	J	=	0.031 in ⁴
Web Thick	=	0.125 in	S _{xx}	=	1.77 in ³	C _w	=	0.78 in ⁶
Flange Width	=	1.520 in	R _{xx}	=	1.620 in	R _o	=	1.970 in
Flange Thick	=	0.296 in	Z _x	=	2.050 in ³	H	=	0.727 in
Area	=	1.340 in ²	I _{yy}	=	0.265 in ⁴	W _{no}	=	1.550 in ²
Weight	=	4.500 plf	S _{yy}	=	0.253 in ³	Sw	=	0.193 in ⁴
Kdesign	=	0.750 in	R _{yy}	=	0.445 in	Q _f	=	0.765 in ³
			Z _y	=	0.495 in ³	Q _w	=	1.010 in ³
rts	=	0.506 in				W _{n2}	=	0.000
Ycg	=	2.000 in				Sw ₂	=	0.088
Xcg	=	0.473 in				Sw ₃	=	0.044
Xp	=	0.305 in						
Eo	=	0.556 in						



Steel Beam

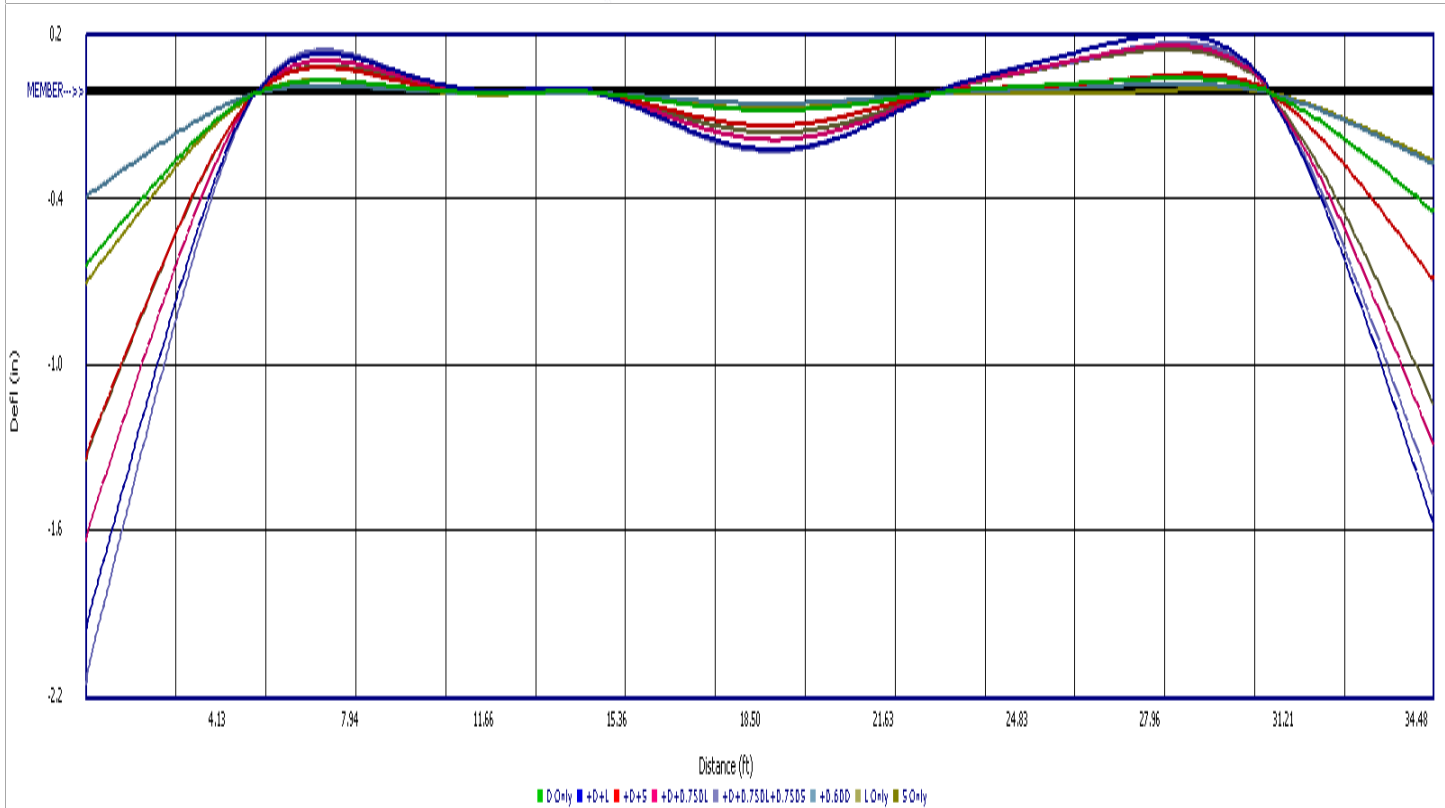
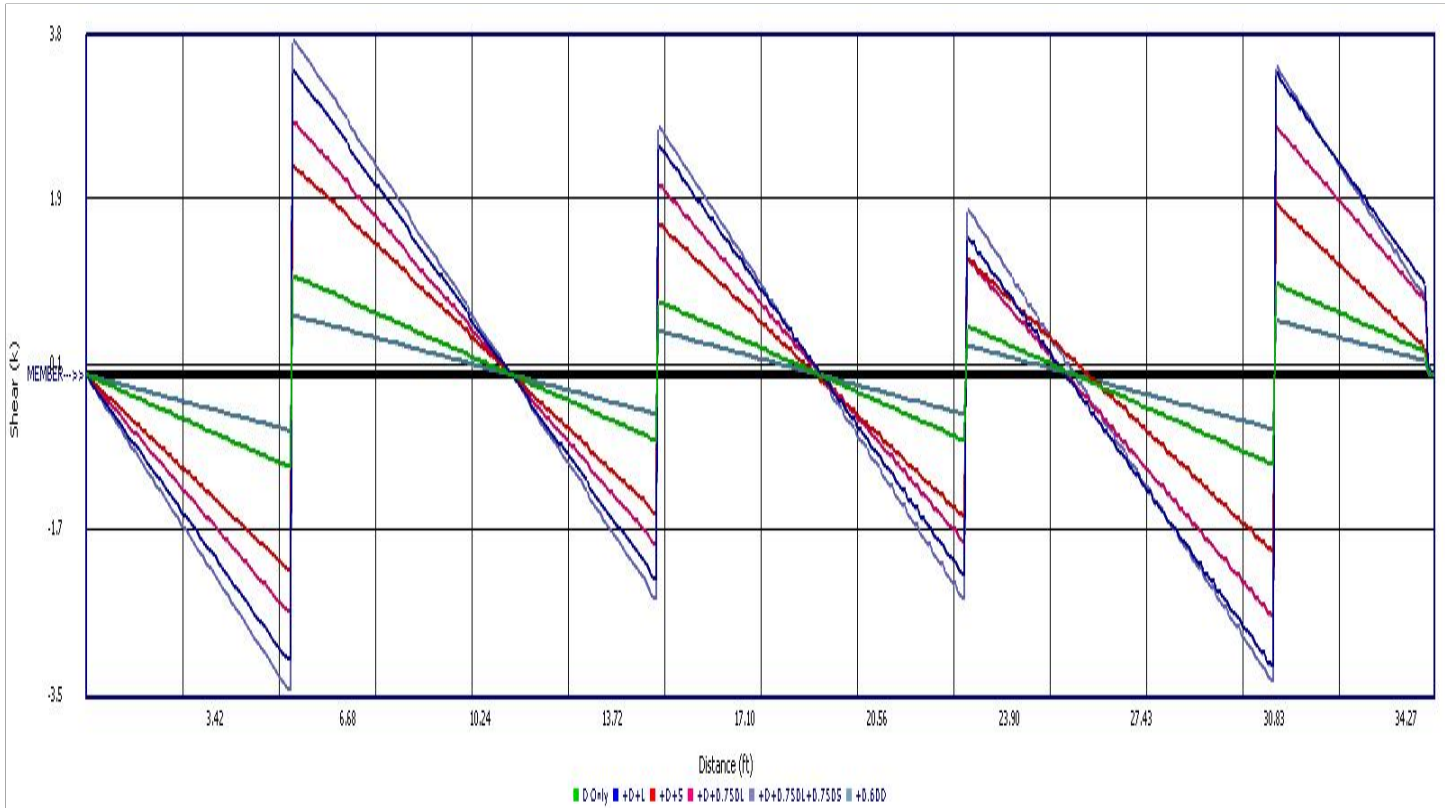
Project File: Liu.ec6

LIC# : KW-06012482, Build:20.23.2.14

Davido Consulting Group

(c) ENERCALC INC 1983-2022

DESCRIPTION: C4x4.5 Pile Cap Type 2



Steel Beam

Project File: Liu.ec6

LIC# : KW-06012482, Build:20.23.2.14

Davido Consulting Group

(c) ENERCALC INC 1983-2022

DESCRIPTION: C4x4.5 Pile Cap Type 3

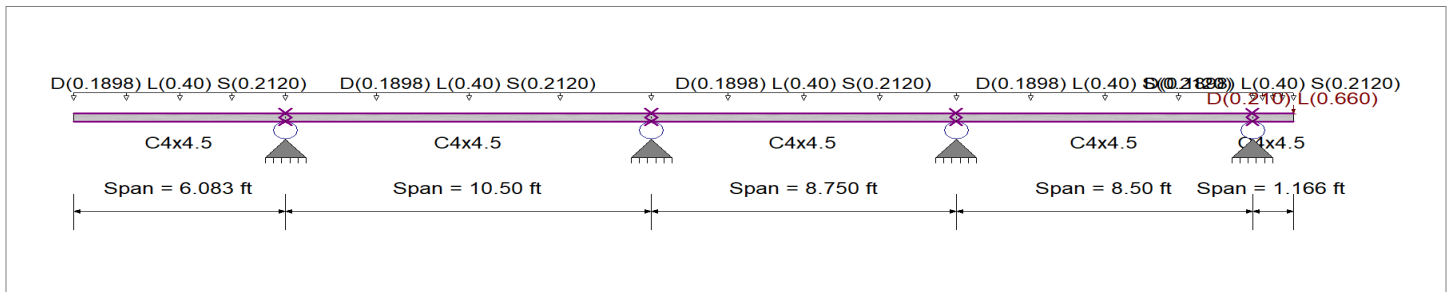
CODE REFERENCES

Calculations per AISC 360-16, IBC 2018, CBC 2019, ASCE 7-16
 Load Combination Set : IBC 2021

Material Properties

Analysis Method Allowable Strength Design
 Beam Bracing : Beam is Fully Braced against lateral-torsional buckling
 Bending Axis : Major Axis Bending

Fy : Steel Yield : 50.0 ksi
 E: Modulus : 29,000.0 ksi



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight NOT internally calculated and added

Load for Span Number 1

Uniform Load : D = 0.1898, L = 0.40, S = 0.2120 k/ft, Tributary Width = 1.0 ft

Load for Span Number 2

Uniform Load : D = 0.1898, L = 0.40, S = 0.2120 k/ft, Tributary Width = 1.0 ft

Load for Span Number 3

Uniform Load : D = 0.1898, L = 0.40, S = 0.2120 k/ft, Tributary Width = 1.0 ft

Load for Span Number 4

Uniform Load : D = 0.1898, L = 0.40, S = 0.2120 k/ft, Tributary Width = 1.0 ft

Load for Span Number 5

Uniform Load : D = 0.1898, L = 0.40, S = 0.2120 k/ft, Tributary Width = 1.0 ft

Point Load : D = 0.210, L = 0.660 k @ 1.166 ft

**Timber Cap + Double Channel
 DCR = 0.923**

DESIGN SUMMARY

Design N.G.

Maximum Bending Stress Ratio =	2.347 : 1	Maximum Shear Stress Ratio =	0.471 : 1
Section used for this span	C4x4.5	Section used for this span	C4x4.5
Ma : Applied	12.005 k-ft	Va : Applied	4.234 k
Mn / Omega : Allowable	5.115 k-ft	Vn/Omega : Allowable	8.982 k
Load Combination	+D+0.750L+0.750S	Load Combination	+D+0.750L+0.750S
Span # where maximum occurs	Span # 1	Location of maximum on span	6.083 ft
		Span # where maximum occurs	Span # 1
Maximum Deflection			
Max Downward Transient Deflection	2.211 in Ratio = 66 >=	Span: 5 : L Only	
Max Upward Transient Deflection	-0.054 in Ratio = 519 >=	Span: 5 : L Only	
Max Downward Total Deflection	3.582 in Ratio = 41 >=	Span: 5 : +D+0.750L+0.750S	
Max Upward Total Deflection	-0.111 in Ratio = 251 >=	Span: 5 : +D+0.750L+0.750S	

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios		Summary of Moment Values					Summary of Shear Values				
			M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx/Vnx/Omega	
D Only														
Dsgn. L =	6.08 ft	1	0.687	0.138		-3.51	3.51	8.54	5.11	1.00	1.00	1.24	15.00	8.98
Dsgn. L =	10.50 ft	2	0.687	0.138	0.53	-3.51	3.51	8.54	5.11	1.00	1.00	1.24	15.00	8.98
Dsgn. L =	8.75 ft	3	0.279	0.104	0.62	-1.43	1.43	8.54	5.11	1.00	1.00	0.93	15.00	8.98

Steel Beam

Project File: Liu.ec6

LIC# : KW-06012482, Build:20.23.2.14

Davido Consulting Group

(c) ENERCALC INC 1983-2022

DESCRIPTION: C4x4.5 Pile Cap Type 3

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios		Summary of Moment Values					Summary of Shear Values				
			M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega Cb	Rm	Va Max	Vnx/Vnx/Omega		
Dsgn. L =	8.50 ft	4	0.279	0.104	0.85	-1.43	1.43	8.54	5.11	1.00	1.00	0.93	15.00	8.98
Dsgn. L =	1.17 ft	5	0.073	0.048		-0.37	0.37	8.54	5.11	1.00	1.00	0.43	15.00	8.98
+D+L														
Dsgn. L =	6.08 ft	1	2.134	0.428		-10.91	10.91	8.54	5.11	1.00	1.00	3.85	15.00	8.98
Dsgn. L =	10.50 ft	2	2.134	0.428	1.63	-10.91	10.91	8.54	5.11	1.00	1.00	3.85	15.00	8.98
Dsgn. L =	8.75 ft	3	0.855	0.318	1.96	-4.37	4.37	8.54	5.11	1.00	1.00	2.85	15.00	8.98
Dsgn. L =	8.50 ft	4	0.855	0.318	2.54	-4.37	4.37	8.54	5.11	1.00	1.00	2.85	15.00	8.98
Dsgn. L =	1.17 ft	5	0.277	0.173		-1.42	1.42	8.54	5.11	1.00	1.00	1.56	15.00	8.98
+D+S														
Dsgn. L =	6.08 ft	1	1.454	0.292		-7.43	7.43	8.54	5.11	1.00	1.00	2.62	15.00	8.98
Dsgn. L =	10.50 ft	2	1.454	0.292	1.13	-7.43	7.43	8.54	5.11	1.00	1.00	2.62	15.00	8.98
Dsgn. L =	8.75 ft	3	0.605	0.224	1.30	-3.09	3.09	8.54	5.11	1.00	1.00	2.01	15.00	8.98
Dsgn. L =	8.50 ft	4	0.605	0.224	1.94	-3.09	3.09	8.54	5.11	1.00	1.00	2.01	15.00	8.98
Dsgn. L =	1.17 ft	5	0.101	0.076		-0.52	0.52	8.54	5.11	1.00	1.00	0.68	15.00	8.98
+D+0.750L														
Dsgn. L =	6.08 ft	1	1.772	0.356		-9.06	9.06	8.54	5.11	1.00	1.00	3.20	15.00	8.98
Dsgn. L =	10.50 ft	2	1.772	0.356	1.36	-9.06	9.06	8.54	5.11	1.00	1.00	3.20	15.00	8.98
Dsgn. L =	8.75 ft	3	0.711	0.264	1.63	-3.64	3.64	8.54	5.11	1.00	1.00	2.37	15.00	8.98
Dsgn. L =	8.50 ft	4	0.711	0.264	2.12	-3.64	3.64	8.54	5.11	1.00	1.00	2.37	15.00	8.98
Dsgn. L =	1.17 ft	5	0.226	0.142		-1.15	1.15	8.54	5.11	1.00	1.00	1.28	15.00	8.98
+D+0.750L+0.750S														
Dsgn. L =	6.08 ft	1	2.347	0.471		-12.00	12.00	8.54	5.11	1.00	1.00	4.23	15.00	8.98
Dsgn. L =	10.50 ft	2	2.347	0.471	1.81	-12.00	12.00	8.54	5.11	1.00	1.00	4.23	15.00	8.98
Dsgn. L =	8.75 ft	3	0.955	0.354	2.13	-4.88	4.88	8.54	5.11	1.00	1.00	3.18	15.00	8.98
Dsgn. L =	8.50 ft	4	0.955	0.354	2.93	-4.88	4.88	8.54	5.11	1.00	1.00	3.18	15.00	8.98
Dsgn. L =	1.17 ft	5	0.247	0.163		-1.26	1.26	8.54	5.11	1.00	1.00	1.46	15.00	8.98
+0.60D														
Dsgn. L =	6.08 ft	1	0.412	0.083		-2.11	2.11	8.54	5.11	1.00	1.00	0.74	15.00	8.98
Dsgn. L =	10.50 ft	2	0.412	0.083	0.32	-2.11	2.11	8.54	5.11	1.00	1.00	0.74	15.00	8.98
Dsgn. L =	8.75 ft	3	0.168	0.062	0.37	-0.86	0.86	8.54	5.11	1.00	1.00	0.56	15.00	8.98
Dsgn. L =	8.50 ft	4	0.168	0.062	0.51	-0.86	0.86	8.54	5.11	1.00	1.00	0.56	15.00	8.98
Dsgn. L =	1.17 ft	5	0.044	0.029		-0.22	0.22	8.54	5.11	1.00	1.00	0.26	15.00	8.98

Vertical Reactions

Support notation : Far left is #

Values in KIPS

Load Combination	Support 1	Support 2	Support 3	Support 4	Support 5	Support 6
Max Upward from all Load Conditions		8.181	5.238	6.201	3.793	
Max Upward from Load Combinations		8.181	5.238	6.201	3.793	
Max Upward from Load Cases		5.042	3.240	3.775	2.603	
D Only		2.393	1.532	1.813	1.114	
+D+L		7.435	4.773	5.588	3.717	
+D+S		5.068	3.233	3.889	2.083	
+D+0.750L		6.175	3.963	4.644	3.066	
+D+0.750L+0.750S		8.181	5.238	6.201	3.793	
+0.60D		1.436	0.919	1.088	0.668	
L Only		5.042	3.240	3.775	2.603	
S Only		2.675	1.700	2.076	0.969	

Steel Beam

Project File: Liu.ec6

LIC# : KW-06012482, Build:20.23.2.14

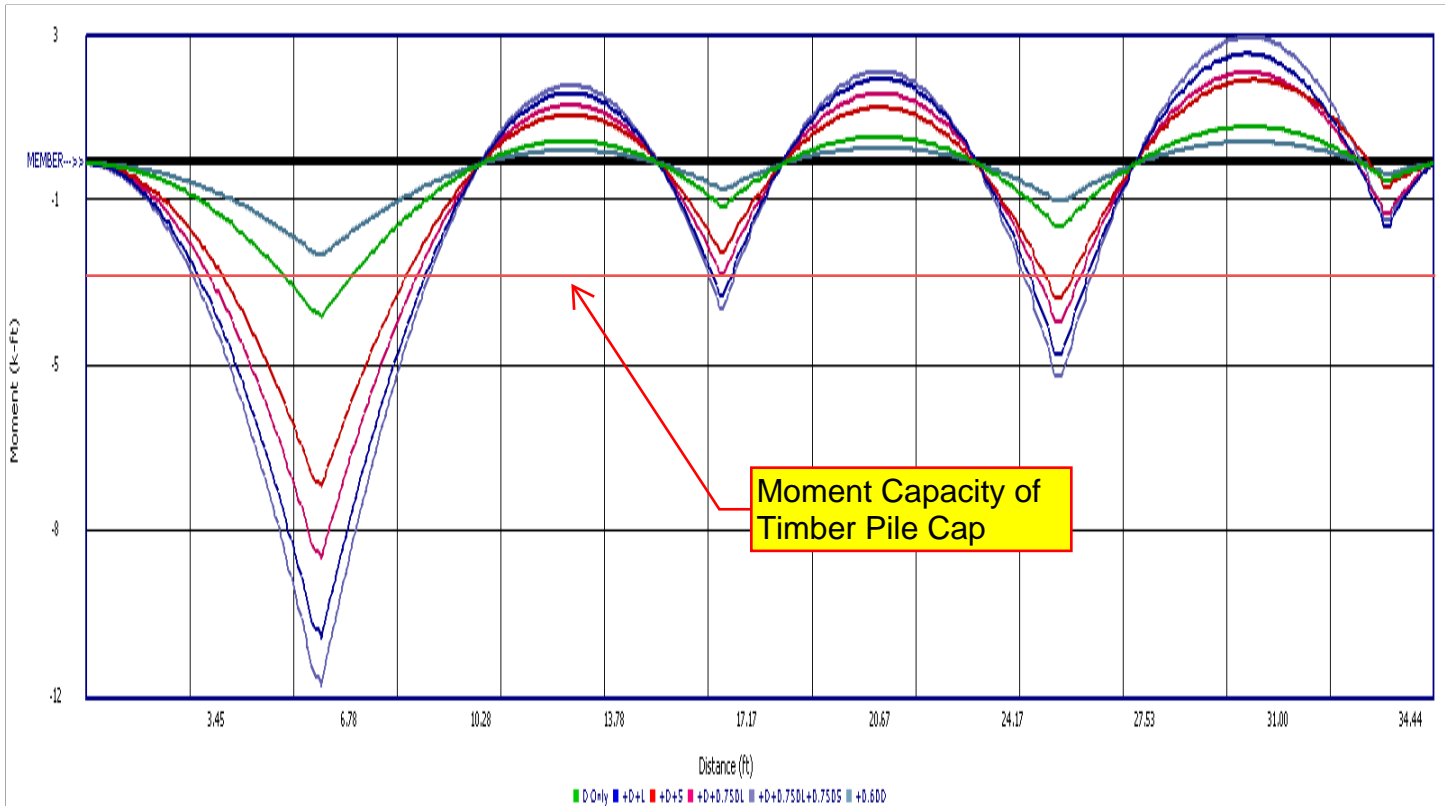
Davido Consulting Group

(c) ENERCALC INC 1983-2022

DESCRIPTION: C4x4.5 Pile Cap Type 3

Steel Section Properties : C4x4.5

Depth	=	4.000 in	I _{xx}	=	3.53 in ⁴	J	=	0.031 in ⁴
Web Thick	=	0.125 in	S _{xx}	=	1.77 in ³	C _w	=	0.78 in ⁶
Flange Width	=	1.520 in	R _{xx}	=	1.620 in	R _o	=	1.970 in
Flange Thick	=	0.296 in	Z _x	=	2.050 in ³		=	0.727 in
Area	=	1.340 in ²	I _{yy}	=	0.265 in ⁴	W _{no}	=	1.550 in ²
Weight	=	4.500 plf	S _{yy}	=	0.253 in ³	Sw	=	0.193 in ⁴
Kdesign	=	0.750 in	R _{yy}	=	0.445 in	Q _f	=	0.765 in ³
			Z _y	=	0.495 in ³	Q _w	=	1.010 in ³
rts	=	0.506 in				W _{n2}	=	0.000
Ycg	=	2.000 in				Sw ₂	=	0.088
Xcg	=	0.473 in				Sw ₃	=	0.044
Xp	=	0.305 in						
Eo	=	0.556 in						



Steel Beam

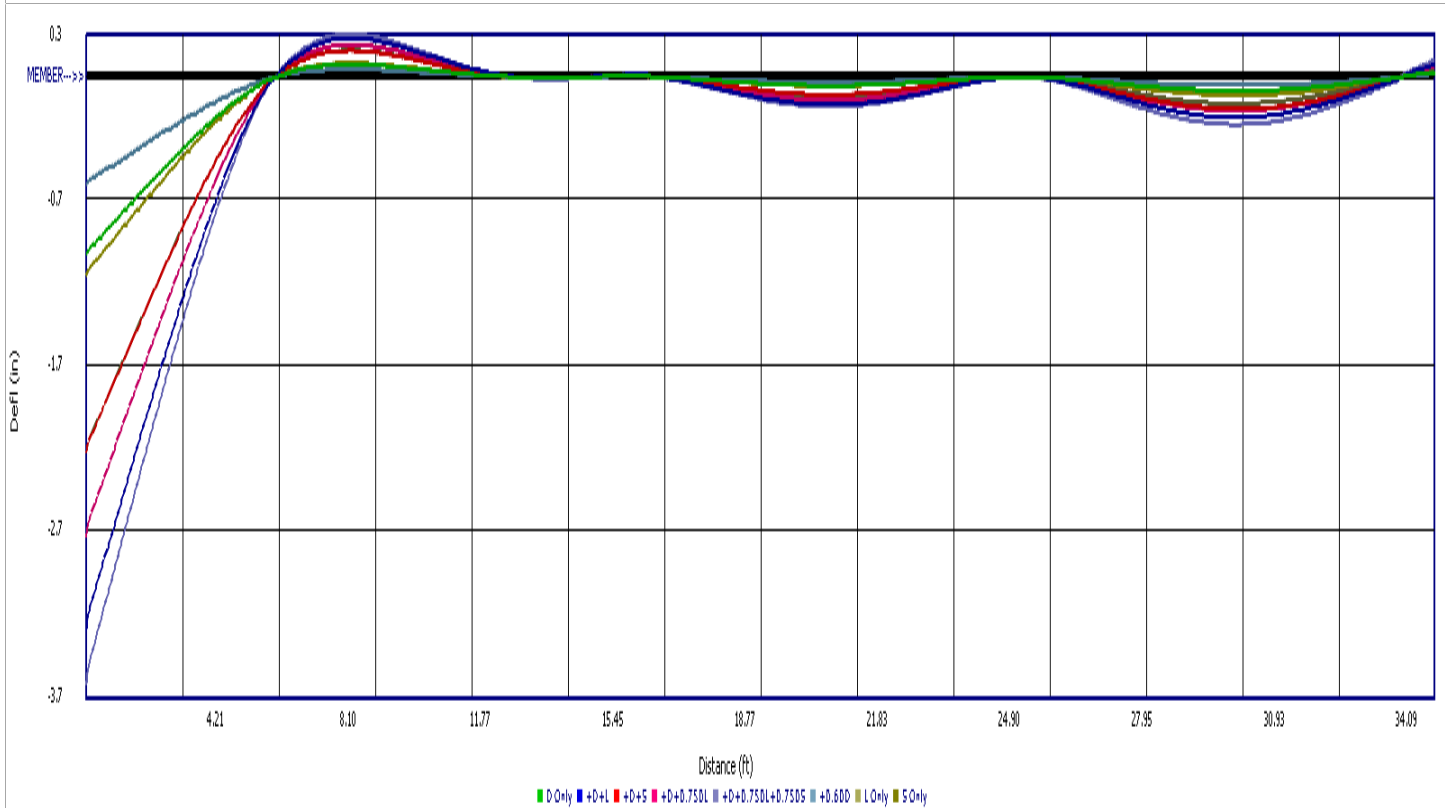
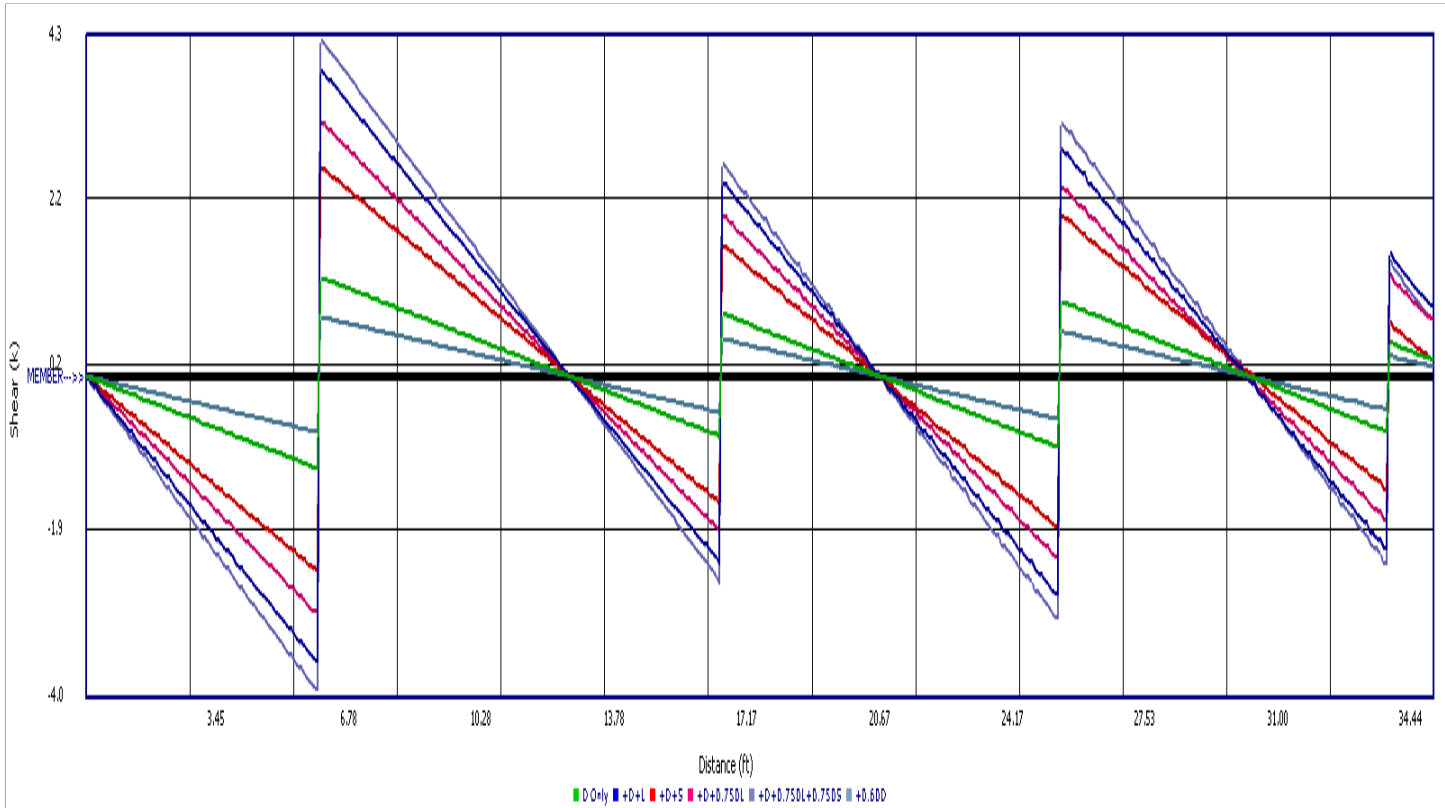
Project File: Liu.ec6


LIC# : KW-06012482, Build:20.23.2.14

Davido Consulting Group

(c) ENERCALC INC 1983-2022

DESCRIPTION: C4x4.5 Pile Cap Type 3



	Seaborn Pile Driving Lake Washington Timber Pile Cap Analysis	Calculations Prepared For Seaborn Pile Driving 7/14/2023
Prepared By: D. Truong Reviewed By: J. Smoot	7422 East Mercer Way, Mercer Island, WA	Double Channel Connection

3/4" Thru-Bolt Shear Capacity (NDS 2015)

ZL	NDS Table 12G G=0.46	1780 lbs
CD	Live Load NDS Table 2.3.2	1
CM	NDS Table 11.3.3	1
Ct	T<100, NDS Table 11.3.4	1

Cg and CA Calculation

n	number of bolts	1	s	Spacing	24	in	
Em	Main Member Elasticity	1300	ksi	D	Bolt Diameter	0.75	in
ES	Steel Elasticity	29000	ksi	γ	Load/Slip Modulus	175370	
Am	Main Member Area	53.8	in ²	u		176.22	
tsteel	Steel Member Thickness	0.125	in	m		0.00	
hsteel	Height of Member	4.0	in	REA		0.21	
As	Area of Steel Member	0.50	in ²				
CA	Geometry Factor					1	
Cg	Group Action Factor					1.00	

End Distance Table 12.5.1A Load ⊥ to grain

End Distance	3.5	in
Min. End Dist. CΔ=1	3	in 4D
Min. End Dist. CΔ=0.5	1.5	in 2D

Spacing Table 12.5.1B Load ⊥ to grain

Bolt Spacing	24	in
Min Spacing	2.25	in 3D

***** Edge Distance Table 12.5.1C Load ⊥ to grain *****

Edge Distance	2	in
Min. Edge Distance, 1.5D Unloaded Edge	1.125	in

Ceg	End Grain Factor	1
Cdi	Diaphragm Factor	1
Ctn	Toe Nail Factor	1

Z'	Capacity of Single Fastener	1.78	kips
Z''	Total Capacity	1.78	kips
	Line Load from Uniform and Point Load	0.9	klf
Zu	Load on Bolt Connection	0.9	kip
DCR	Demand to Capacity Ratio	0.49	



****For Bolt Demand, take uniform load from all load sources and multiply by bolt spacing, divide by 2 for two channels**